# Exhibit 5

<u>February 12, 2019 Revised NPDES Renewal Application</u> <u>for Starkist Samoa Co. (AS0000019)</u>



February 12, 2019

Tomas Torres, Director Water Division – Region 9 U.S. Environmental Protection Agency 75 Hawthorne Street San Francisco, CA 94105

RE: Revised NPDES Renewal Application for StarKist Samoa Co. (AS0000019)

Dear Mr. Torres:

Enclosed please find completed Form 1 and Form 2C for the renewal of the current NPDES permit (Permit No. AS0000019) StarKist Samoa Co. (StarKist), which expired on March 31, 2013 (the effective permit). The application for permit renewal was submitted on time (September 17, 2012) and the effective permit was administratively extended. At the request of U.S. Environmental Protection Agency (U.S. EPA), an updated complete permit renewal application was submitted on April 29, 2016. An updated request for a water quality certification and mixing zone analysis (MZA) was also submitted to the American Samoa Environmental Protection Agency (ASEPA) in February 2017.

Following submittal of the permit renewal application in April 2016, no draft NPDES permit was developed. In 2016 and 2017, the Facility implemented numerous upgrades and changes to treatment processes. The characterization of water quality from the WWTP effluent, as described in Form 2C of the April 2016 permit renewal application, reflected the most recent water quality data available at the time of the application development (in early 2016) and did not reflect improvements to the final effluent wastewater quality at the Facility achieved via the various upgrades and changes. Because of these modifications to treatment processes and resulting changes in effluent water quality at the Facility, StarKist submitted an amended NPDES permit renewal application on January 31, 2018 to reflect these improvements and changes. Additional effluent characterization information was then submitted in August 2018 to better characterize the improved effluent water quality due to the facility upgrades (most notably, water quality improvements due to implementation of the evaporators in late 2017).



StarKist has also performed additional receiving water sampling in 2018, beyond the permit required semi-annual sampling. These sampling events have shown that American Samoa Water Quality Standards (ASWQS) have been met in the receiving water in 2018 and represent a significant improvement from past sampling results prior to 2018, particularly with respect to nutrients. This improvement in receiving water quality is timed with, and believed to be the result of, recent wastewater treatment improvements at StarKist.

A pre-public draft permit for StarKist was issued on September 18, 2018, and StarKist provided comments on the pre-public draft permit on October 5, 2018. During discussions with U.S EPA and ASEPA, resuming ocean disposal of tuna processing waste was identified by the agencies as a potential option that StarKist was encouraged to pursue. StarKist was previously authorized by U.S EPA Region 9 to dispose of fish waste at an offshore location (the site was designated as a disposal site in February 1990).

StarKist has decided to pursue resuming ocean disposal of a portion of the tuna processing waste generated at the Facility and is currently coordinating with the Ocean Dumping Management Program at U.S EPA Region 9. StarKist plans to resume ocean disposal of certain of the wastewater streams that were historically sent to ocean disposal.

Resuming ocean dumping for a portion of the tuna processing wastewater will affect the wastewater that is treated and discharged through the Joint Cannery Outfall (JCO) into Pago Pago Harbor. The characterization of water quality from the wastewater treatment plant (WWTP) effluent to be discharged through the JCO will be significantly different with the inclusion of ocean disposal, ultimately reducing the flowrates, concentrations, and loads discharged through the JCO. As a result, the amended NPDES permit renewal application submitted on January 31, 2018 is no longer representative of anticipated discharge conditions during the next permit term. StarKist has further amended the NPDES permit renewal application to reflect the implementation of ocean disposal for a portion of the tuna processing waste.

As previously mentioned, StarKist is concurrently seeking approval to resume ocean disposal of certain wastewater streams that were historically ocean disposed. StarKist was not been able to coordinate with U.S EPA Region 9 regarding whether the historical wastewater streams continue to be acceptable for ocean disposal, due to the thirty-five day partial shutdown of the U.S. government that started on December 22, 2018. The NPDES permit renewal application has been amended with the assumption that ocean disposal will be resumed for wastewater streams that were previously sent to ocean disposal. If changes are required to the tuna processing waste sent to ocean disposal, this will further affect the quality and quantity of treated wastewater



discharged through the JCO and amended information will be provided to U.S. EPA. Similarly, if ocean disposal is not approved, or contributions to ocean disposal are restricted, the loading to the JCO discharge will change.

The items that have been amended since submittal of the permit renewal application in January 2018 include the following:

- Descriptions of operations and treatment processes (Part II of Form 2C, included in Attachment A), including wastewater streams planned for ocean disposal
- Process flow diagrams (Part II of Form 2C, included in Figures P101 and P102)
- Effluent Characteristics<sup>1</sup> (Part V of Form 2C)

The current NPDES permit limitations for total nitrogen (TN) and total phosphorus (TP) were determined based on a historical agreement between StarKist and Samoa Tuna Processors (STP) that apportioned the total allowable load from the JCO between the two canneries based on each facility's need. The allowed JCO load for ammonia was also apportioned between facilities. StarKist and STP negotiated a revised apportionment of the total allowable ammonia, TN and TP load for each cannery to reflect the needs of each facility over the upcoming permit term. This agreement was made on May 16, 2018 and was provided to U.S. EPA.

After discussions with U.S. EPA related to the MZA submitted in 2017 and the pre-public draft permit, and given new plans for ocean disposal of certain allowed waste streams, StarKist is now requesting permit limits for nutrients (total nitrogen and total phosphorus) – when summed to a total combined allowable load to the JCO (from both SKS and STP) —that are consistent with the current permits for the two facilities, reapportioned appropriately between StarKist and STP.

<sup>&</sup>lt;sup>1</sup> Effluent data was updated for total aluminum, ammonia as nitrogen, biological oxygen demand (5 day), total cadmium, chemical oxygen demand, total chromium, total copper, total mercury, total nickel, nitrate+nitrite (as N), total nitrogen, oil and grease, total phosphorus, total suspended solids, and flow. Because ocean disposal has not yet been resumed, historical water quality data reflecting this condition are not available. Therefore, the effluent characterization for the aforementioned parameters represents calculated estimates of anticipated effluent quality (described in further detail in Attachment A).



Therefore, no change to the existing permits' combined total allowed loads to the JCO is requested.<sup>2</sup>

All subsequent information presented herein was provided in the transmittal letter with the January 2018 permit renewal application materials and has only been updated with more current information as appropriate.

Results of monitoring performed during the effective permit have been submitted to the U.S. Environmental Protection Agency (U.S. EPA) Region 9. A summary of monitoring, including pending reports currently under development, include:

- **Discharge Monitoring Reports (DMRs):** StarKist has been submitting routine DMRs as required by the effective NPDES permit. The most recent DMR, which includes data from the fourth quarter of 2018, was submitted on January 15, 2019.
- **Priority Pollutant Scan (PPS):** sampling for the PPS was performed in February 2016, and the results are included in the amended permit renewal application as appropriate (section V of Form 2C). A PPS report was submitted to U.S. EPA May 23, 2016.
- Semi-annual toxicity effluent monitoring: effluent monitoring has been performed semi-annually, as required by the effective permit. The most recent JCO effluent toxicity testing was performed in August 2018, and results are included in the amended permit renewal application as appropriate (section V of Form 2C).
- Semi-annual receiving water monitoring: receiving water monitoring has been performed and reported as required by the effective permit. Additionally, supplemental sampling has been performed at selected stations in 2018 to confirm whether recent receiving water quality improvements were being maintained and to expand the 2018 dataset. The most recent receiving water sampling was completed in December 2018. Results from the December 2018 sampling event were pending at the time the permit application was prepared; however, results from October 2018 have been submitted to U.S. EPA. Results from the multiple receiving water quality sampling events since March 2018 have shown the receiving water to be in compliance with applicable water quality standards.

<sup>&</sup>lt;sup>2</sup> In the event that U.S. EPA disagrees with procedure of reallocating the nutrient loads between the StarKist and STP facilities, StarKist nevertheless seeks authorization for and issuance of an NPDES permit with similar discharge limits to those sought via the reapportionment described above, under the basis that such final effluent limits are independently justifiable on the basis of the accompanying NPDES permit application and on mixing zone modeling.



The following additional supplemental information was requested by Mr. Pascal Mues during a phone discussion on March 28, 2016 and was previously included with the renewal application dated April 29, 2016 (Attachment A). This information has been updated as appropriate in the amended permit renewal application now being submitted:

- An evaluation of the metals Pollutant Minimization Plan (PMP) that was submitted by Glatzel Da Costa (gdc) (December 14, 2010 and supplemented on July 28, 2011) to fulfill special conditions submittal requirements of the effective NPDES permit is being updated in Attachment A. This evaluation includes a description of actions implemented at the facility based on the PMP, evaluation of the effectiveness of these measures, determination if further actions are needed based on current water quality conditions at the Facility (i.e., post-high strength wastewater and treatment upgrades), and an informal assessment of whether permit requirements were met.
- Nutrient PMP (or "Action Plan"), which is not required per the effective permit but was
  requested through communication with Mr. Mues, is also being updated in Attachment A.
  The requested information included a summary of the Environmental Summary Report
  submitted to the U.S. EPA in December 2015 and improvements completed since the
  report was issued. This information includes actions that StarKist plans to implement to
  reduce nutrients in the effluent and the timeline for implementation of these actions.

The effective permit also required submittal of certain studies as part of the special conditions, which included the following items that were previously submitted:

- Nutrient Assessment that addresses dilution calculations, waste load allocation estimates, model input/output, and an evaluation of the existing size of the mixing zone for nutrients based on modeling. Sampling was conducted in February 2010, September 2010, October 2010, and March 2011, and reports for these sampling events were submitted on June 9, 2010, December 6, 2010, and August 1, 2011, respectively. The effective permit also required a Nutrient Assessment workplan that describes a process to assess nutrients in the combined discharge, and the dilution required to meet water quality standards. The draft workplan was submitted with the June 9, 2010 report.
- A chronic toxicity special study to evaluate chronic toxicity levels of the combined cannery effluent after initial mixing in the receiving water, under critical conditions, and subsequent dilution. Semi-annual chronic toxicity testing was required to determine levels of chronic toxicity in the discharge, the appropriate dilution ratio using range finding test procedures, and effluent triggers or limits. The Chronic Toxicity Study Report was submitted to U.S. EPA and ASEPA on August 1, 2011.



We look forward to working with U.S. EPA and ASEPA in the development of the renewed NPDES permit. If you have any questions or require additional information, please feel free to contact us at your convenience. Thank you for your consideration.

I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gather and evaluate the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

Sincerely,

Kwon Sangdong General Manager

Attachments:

Form 1

Form 2C

Figure P101

Figure P102

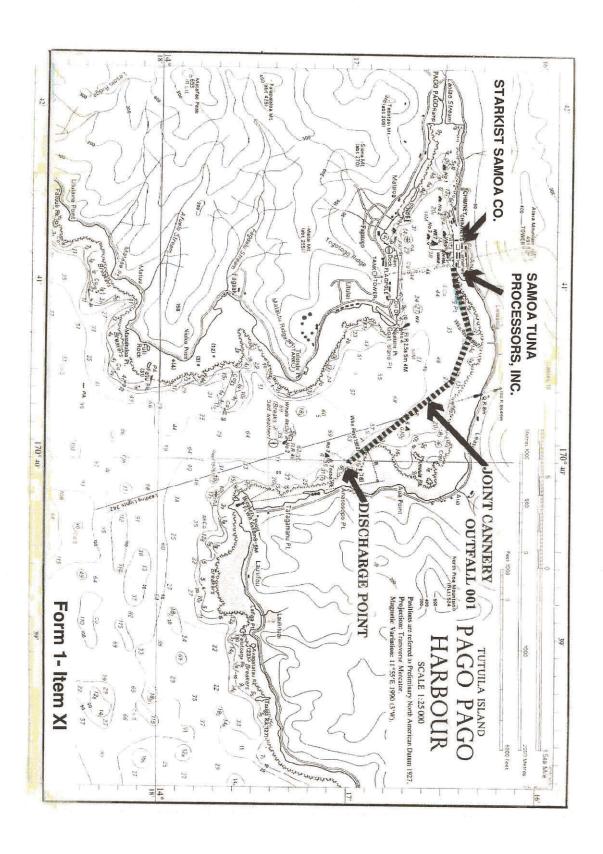
Attachment A – NPDES Application Form 2C Supplemental Materials

INSTRUCTIONS: Complete A through J to determine whether you need to submit any permit application forms to the EPA. If you answer "yes" to any questions, you must submit this form and the supplemental form listed in the parenthesis following the question. Mark "X" in the box in the third column if the supplemental form is attached. If you answer "no" to each question, you need not submit any of these forms. You may answer "no" if your activity is excluded from permit requirements; see Section C of the instructions. See also, Section D of the instructions for definitions of **bold-faced terms**.

II. POLLUTANT CHARACTERISTICS

		Mari	( "X"				Mari	k "X"
SPECIFIC QUESTIONS	YES	NO	FORM ATTACHED		SPECIFIC QUESTIONS	YES	NO	FORM ATTACHED
A. Is this facility a publicly owned treatment works which results in a discharge to waters of the U.S.? (FORM 2A)	16	X	18	inc aq	pes or will this facility (either existing or proposed) clude a concentrated animal feeding operation or quatic animal production facility which results in a scharge to waters of the U.S.? (FORM 2B)	19	X 20	21
C. Is this a facility which currently results in <b>discharges</b> to waters of the U.S. other than those described in A or B above? (FORM 2C)	X		X	D. Is	this a proposed facility (other than those described in A B above) which will result in a discharge to waters of e U.S.? (FORM 2D)	19	X	21
TO CONTRACT TO CONTRACT	22	23	24	Cit	e 0.3.? (FORWI 2D)	25	26	27
E. Does or will this facility treat, store, or dispose of hazardous wastes? (FORM 3)	28	X 29	30	co	o you or will you inject at this facility industrial or unicipal effluent below the lowermost stratum intaining, within one quarter mile of the well bore, iderground sources of drinking water? (FORM 4)	31	×	
G. Do you or will you inject at this facility any produced water or other fluids which are brought to the surface in connection with conventional oil or natural gas production, inject fluids used for enhanced recovery of oil or natural gas, or inject fluids for storage of liquid hydrocarbons? (FORM 4)	34	×		pro	o you or will you inject at this facility fluids for special occesses such as mining of sulfur by the Frasch process, lution mining of minerals, in situ combustion of fossil el, or recovery of geothermal energy? (FORM 4)		×	33
I le this facility a server of at at	34	35	36	2 27		37	38	39
<ol> <li>Is this facility a proposed stationary source which is one of the 28 industrial categories listed in the instructions and which will potentially emit 100 tons per year of any air pollutant regulated under the Clean Air Act and may affect</li> </ol>		×		NC ins ye:	this facility a proposed <b>stationary source</b> which is DT one of the 28 industrial categories listed in the structions and which will potentially emit 250 tons per ar of any air pollutant regulated under the Clean Air Act		×	
or be located in an attainment area? (FORM 5)	40	41	42		d may affect or be located in an attainment area? ORM 5)	43	44	45
III. NAME OF FACILITY			20 BIOS				TO ST	Tion cause
1 SKIP StarKist Samoa Co.			TII			Territoria		
15 16 - 29 30						69		
IV. FACILITY CONTACT			445545		The state of the s			
A. NAME & TITLE (last	first	& title)			B BHONE (annual of the N			
2 John Dearness		TT		П	B. PHONE (area code & no.) (684) 258-3234			
15 16					45 46 48 49 51 52- 5	5		
V.FACILTY MAILING ADDRESS	A	TOP	HAPP		A CROST BY THE SHAPE SHOW			
A. STREET OR P.	0. во	X	111	11				
3 P.O. Box 368					45			
B. CITY OR TOWN					C. STATE D. ZIP CODE			
4 Pago Pago	Т	П	1 1 1	П	AS 96799			
15 16					40 41 42 47 51			
VI. FACILITY LOCATION				380	PART HIS TONE OF THE SAME			Zykst.
A. STREET, ROUTE NO. OR OTHE	RSPE	CIFIC	IDENTIFIE	R				
5 368 Atu'u Road		1 1						
15 16					45			
B. COUNTY Maoputasi	NAME		П	П				
46 COLTY OF TOWAR					70		C1.	1
C. CITY OR TOWN	11	Т	ПП	1 1	D. STATE E. ZIP CODE F. COUNTY CO	DE (ij	know	1)
15 16					40 41 42 47 51 52	-54		
EPA Form 3510-1 (8-90)						UNITA	E ON	REVERSE

CONTINUED FROM THE FRONT		
VII. SIC CODES (4-digit, in order of priority)	A CHARLES IN THE REST.	
A. FIRST  c (specify) Processing and canning of tuna fish		B. SECOND
7 2091 (************************************	7 2048 (specify) Processing	g of fish by-product into fish meal
15 16 - 19	15 16 - 19	
C. THIRD  (specify) Canning of pet food (not currently don	or the GIIII	D. FOURTH
7 204 / facility)	e at the c (specify)	
15 16 - 19	15 16 - 19	
VIII. OPERATOR INFORMATION	NAME	
	NAME I I I I I I I I I I I I I I I I I I I	B.Is the name listed in Item VIII-A also the owner?
8 StarKist Samoa Co.		☐ YES ☑ NO
		55 66
	riate letter into the answer box: if "Other," specify.)	D. PHONE (area code & no.)
F = FEDERAL S = STATE M = PUBLIC (other than federal or	state) P (specify)	a (684) 622-2025
P = PRIVATE O = OTHER (specify)		
F OTBETT OF D C 2004	56	15 6 - 18 19 - 21 22 - 26
E. STREET OR P.O. BOX		
P.O. Box 368		
26	65	
F. CITY OR TOWN	G. STATE   H.	ZIP CODE IIX, INDIAN LAND
		Is the facility located on Indian lands?
B Pago Pago	AS   96	799 ☐ YES ☑ NO
15 16	40 41 42 47	• 51
X. EXISTING ENVIRONMENTAL PERMITS	P. POP (4. P.	
A. NPDES (Discharges to Surface Water)	D. PSD (Air Emissions from Proposed Sources)	
9 N AS0000019 9 P	Fish Meal Process	
15 16 17 18 30 15 16	17 18	30
B. UIC (Underground Injection of Fluids)	E. OTHER (s	
9 U	2015 MSGP	(specify) Multi-sector General Permit for
9 U 9 15 16 17 18 30 15 16		Stormwater Discharges Associated with Industrial Activity (MSGP)
C. RCRA (Hazardous Wastes)	E. OTHER (s	30   necrfic)
C T I C T		(specify) Minor sourc Air Quality Permits
9 R 9	Boilers 800,600A,B,C,D	issued by American Samoa EPA.
15 16 17 18 30 15 16	17 18	30
XI. MAP		
Attach to this application a topographic map of the area extending location of each of its existing and proposed intake and discharge	to at least one mile beyond property boundaries.	The map must show the outline of the facility, the
injects fluids underground. Include all springs, rivers, and other surfa-	ce water bodies in the map area. See instructions fo	r precise requirements.
XII. NATURE OF BUSINESS (provide a brief description)	CONTRACTOR OF THE PARTY OF THE	
StarKist Samoa conducts the processing and ca	nning of tuna fish and other ingre	edients (water, oil, and salt) for
numan consumption, pet food, and the process	ng of fish by-product into fish me	al StarVist Campais treated
wastewater is discharged through an outfall a Processors). The joint cannery outfall discha	nd diffuser it shares with the adi	oining cannery (Samoa Tuna
Pago Pago Harbor outer reach, in 176 feet of	water.	into marine receiving water, the
Company Consideration Section (Consideration of Section (Consideration Consideration C		
1.		
VIII CERTIFICATION (see instanting		
XIII. CERTIFICATION (see instructions)	The second secon	NAME OF TAXABLE PARTY.
I certify under penalty of law that I have personally examined and a inquiry of those persons immediately responsible for obtaining the am aware that there are significant penalties for submitting false info	nformation contained in the application. I believe that	t the information is true, accurate, and complete 1
A. NAME & OFFICIAL TITLE (type or print)	B. SIGNATURE	C. DATE SIGNED
		)
Sangdong Kwon, General Manager	A	02/11/2019
	1/1/1/	
COMMENTS FOR OFFICIAL USE ONLY		THE REAL PROPERTY AND ADDRESS OF THE PARTY AND
С		



Form Approved. OMB No. 2040-0086. Approval expires 3-31-98.

Please print or type in the unshaded areas only.

FORM **\$EPA** 2C **NPDES** 

U.S. ENVIRONMENTAL PROTECTION AGENCY APPLICATION FOR PERMIT TO DISCHARGE WASTEWATER

EXISTING MANUFACTURING, COMMERCIAL, MINING AND SILVICULTURE OPERATIONS Consolidated Permits Program

A. OUTFALL NUMBER			riodation to t		TO THE RESIDENCE OF THE PARTY O		f the receiving water.
		. LATITUDE		C.	LONGITUDE		
(list)	1. DEG.	2. MIN.	3. SEC.	1. DEG.	2. MIN.	3. SEC.	D. RECEIVING WATER (name)
001	14.00	16.00	49.00	170.00	40.00	8.00	Pago Pago Harbor
							Note: Latitude is South and
							Longitude is West
							Note: Coordinates are for outfall
							diffuser

line drawing showing the water flow through the facility. Indicate sources of intake water, operations contributing wastewater to the effluent, and treatment units labeled to correspond to the more detailed descriptions in Item B. Construct a water balance on the line drawing by showing average flows between intakes, operations, treatment units, and outfalls. If a water balance cannot be determined (e.g., for certain mining activities), provide a pictorial description of the nature and amount of any sources of water and any collection or treatment measures.

B. For each outfall, provide a description of: (1) All operations contributing wastewater to the effluent, including process wastewater, sanitary wastewater, cooling water, and storm water runoff; (2) The average flow contributed by each operation; and (3) The treatment received by the wastewater. Continue on additional sheets if

1. OUT-	2. OPERATION(S)	CONTRIBUTING FLOW	3. TREATMEN	NT
FALL NO. (list)	at of all thort (mil)	b. AVERAGE FLOW (include units)	a. DESCRIPTION	b. LIST CODES FROM TABLE 2C-1
001	See Attachment	See Attachment	See Attachment	
-				
ŀ				
1				
	USE ONLY (effluent guidelines sub-cate			

YES (compl	ete the follo	wing table)			NO (go to See	ction III)				
				3. FF	REQUENCY			4. FLC	DW .	
	2. 0	PERATION(s		a. DAYS PE WEEK	B. MONTHS	a. FLOW RA	ATE (in mgd)		TOTAL VOLUME specify with units)	
1. OUTFALL NUMBER (list)	CONTR	RIBUTING FLO	OW	(specify average)	PER YEAR (specify average)	1. LONG TERM AVERAGE	2. MAXIMUM DAILY	1. LONG	TERM 2. MAX	
III. PRODUCTION	- Unritedia		41.584							
A. Does an effluent guideling  YES (complete)	ete Item III-	B)			NO (go to Sec	tion IV)				
B. Are the limitations in the a	applicable	effluent guid	eline expressed in t	erms of pro	duction (or other NO (go to Sec		ration)?			
C. If you answered "yes" to applicable effluent guidel	Item III-B.	list the qua	ntity which represe	nts an actua	al measurement of	of your level of	production, exp	oressed i	n the terms and	I units used in th
	me, and m	197 (4)	VERAGE DAILY PR						2 AFFECTED	DUTEALLO
a. QUANTITY PER DAY	b. UNITS	OF MEAS	JRE	c. OPERAT	ION, PRODUCT, (specify)	MATERIAL, ET	c.		2. AFFECTED ( (list outfall n	
production (based on April-December 2018) is 446 MT/day.  The anticipated maximum average daily production for the permit term is 552 MT/day.		ons/day	Tuna					001		
V. IMPROVEMENTS	MONEY.			15-25		RH SLIN		10 PER	Mary Mary	Andrew Street
deadness equipment of p	strative or	enforcemen	nvironmental progra	ams which r	meet any implementation schedule for the construction, s which may affect the discharges described in this application compliance schedule letters, stipulations, court orders, and NO (go to Item II'-B)			cation?	hie includes he	it is not limited to
1. IDENTIFICATION OF CO AGREEMENT, ETC		2. AF	FECTED OUTFALL	.s	3. BRIEF I	DESCRIPTION	OF PROJECT		4. FINAL COI	MPLIANCE DAT
AGREEMENT, ETC		a. NO.	b. SOURCE OF DIS	CHARGE					a. REQUIRED	b. PROJECTED
United States District Court Western District Cennsylvania Pittsburg Division. United State Merica v. StarKist Co StarKist Samoa Co. Con Decree	of gh es of o. and	001	Wastewater treatment operations fo processing an canning of tu	r the with the sriid	onsent Decree ivil penalty, astewater con reatment upgur ffluent limit pill preventi egulations, snvestigation ock trench an ssessments, a	evaluation ppliance mean ades, compliance on a count con and count tormwater per of illicit and sump inspect	of interim sures, wast iance with site labora termeasure ermitting a connections ections and	ewater final tory, nd , and	December 31, 2020	December 31 2020
3. OPTIONAL: You may at	took addit	ional sheets	describing any as	(disingular and annual						

EPA Form 3510-2C (8-90)

MARK "X" IF DESCRIPTION OF ADDITIONAL CONTROL PROGRAMS IS ATTACHED

ASD 983 366 030

### V. INTAKE AND EFFLUENT CHARACTERISTICS

A, B, & C: See instructions before proceeding – Complete one set of tables for each outfall – Annotate the outfall number in the space provided. NOTE: Tables V-A, V-B, and V-C are included on separate sheets numbered V-1 through V-9.

D. Use the space below to list any of the pollutants listed in Table 2c-3 of the instructions, which you know or have reason to believe is discharged or may be discharged from any outfall. For every pollutant you list, briefly describe the reasons you believe it to be present and report any analytical data in your possession.

1. POLLUTANT	2. SOURCE	1. POLLUTANT	2. SOURCE
Formaldehyde (contained in Termin-8, which is used in fish meal processing)  Xylene (contained in Demand CS, which is used facility pest control)  Pyrethrins (contained in Sunbugger 100 and Pro-Control, which are used for facility pest control)	All analytical data have been submitted to EPA under existing NPDES Permit requirements.  No analytical data for these pollutants are available. However, Attachment A (Table 1) contains estimated quantities for annual usage of these substances and additional information regarding their potential discharge.  StarKist does maintain material safety data sheets for these chemicals.	Certain substances (listed in Table 20-4 of instructions for this form) are used at the facility and may be discharged. In order to apply for exclusion of the discharges from requirements of section 311 of the CWA, these substances are identified in the Attachment.	See Attachment.

VI.	POTENTIAL	DISCHARGES	NOT	COVERED	BY ANALYSIS

YES (list all such pollutants below)	of a substance which you currently use or manufacture as an intermediate or final product $\boxed{\checkmark}$ NO (go to Item VI-B)	0.000

# CONTINUED FROM THE FRONT

VII. BIOLOGICAL TOXICITY TESTING			
Do you have any knowledge or reason relation to your discharge within the las	to believe that any biological test for acute or chro t 3 years?	onic toxicity has been made on any of you	r discharges or on a receiving water in
	md describe their purposes below)	NO (go to Section VIII	)
The current NPDES Permit 24-hour combined-composit (JCO).	(No. AS0000019) requires semi-an e for effluent from both canneri	nual testing for chronic to es discharging through the	oxicity of a flow-weighted Joint Cannery Outfall
From the effective date o StarKist Samoa (SKS) and	f the permit (April 2008) throug Samoa Packing (COS) effluent.	h 2009, the testing was dor	ne for the combined
Samoa Packing (COS) termi Packing (COS) facility an	nated operations in September 20 d started operations in April 20	09. Samoa Tuna Processors 15. STP ceased operation in	(STP) purchased the Samoa
Starting in September 200 to EPA on a routine basis weighted effluent samples copper, zinc, mercury, am	9, only the StarKist Samoa efflu. Beginning in August 2015, STP of from SKS and STP were used to commonia, total nitrogen, and total aphted samples from each facility.	ent (SKS) was tested, and r was also tested separately reate composite samples the	results have been provided for chronic toxicity. Flow at were analyzed for
VIII. CONTRACT ANALYSIS INFORMA	TION		
	m V performed by a contract laboratory or consult	ting firm?	
	ss, and telephone number of, and pollutants analyzed b	200 B 0 W 10 V	
each such laboratory	or firm below)	y. NO (go to Section IX)	
A. NAME	B. ADDRESS	C. TELEPHONE (area code & no.)	D. POLLUTANTS ANALYZED (list)
TestAmerica, Inc.	17461 Derian Ave #100 Irvine, CA 92614	(949) 261-1022	Ammonia, COD (dissolved and total), O&G, nitrite + nitrate, TN, phosphorus (dissolved and total), TKN (dissolved and total), total solids, TSS, volatile suspended soids, total volatile solids, BOD
ALS Environmental	1317 South 13th Avenue Kelso, WA 98626	(360) 577-7222	JCO effluent toxicity (ammonia, nitrate + nitrite, TKN, total phosphorus, mercury, copper, zinc, and WET) and priority pollutant scan (PPS) data
,			
IX. CERTIFICATION		<b>建设设置,1963年</b>	
directly responsible for gathering the int	ncument and all attachments were prepared under devaluate the information submitted. Based on formation, the information submitted is, to the besi alse information, including the possibility of fine an	my inquiry of the person or persons what t of my knowledge and belief true, accur.	n manage the system or those persons
A. NAME & OFFICIAL TITLE (type or pri		B. PHONE NO. (area code & no.)	
Sangdong Kwon, General Man	ager	(684) 622-2025	
C. SIGNATURE		D. DATE SIGNED	
	300	02/11/2019	
	1/1/		

EPA Form 3510-2C (8-90)

PLEASE PRINT OR TYPE IN THE UNSHADED AREAS ONLY. You may report some or all of this information on separate sheets (use the same format) instead of completing these pages. SEE INSTRUCTIONS.

EPA I.D. NUMBER (copy from Item I of Form I)

OUTFALL NO. ASD 983 366 030 V. INTAKE AND EFFLUENT CHARACTERISTICS (continued from page 3 of Form 2-C)

PART A-You must provide the results of at least one analysis for every pollutant in this table. Complete one table for each outfall. See instructions for additional details.

b. NO. OF ANALYSES (2) MASS 4. INTAKE (optional) a. LONG TERM AVERAGE VALUE (1) CONCENTRATION VALUE VALUE VALUE 1b/day 1b/day 1b/day 1b/day b. MASS 1b/day mgd STANDARD UNITS (specify if blank) 3. UNITS a. CONCENTRATION S ç mg/L mg/L mg/L mg/L mg/L OF/ OF/ d. NO. OF ANALYSES 196 225 113 209 136 196 51 96 Н 29,851 8,076 (2) MASS 757 553 c. LONG TERM AVRG. VALUE (if available) 88.9/31.6 89.9/32.2 1.87 (1) CONCENTRATION 1,909 517 48 35 VALUE VALUE VALUE 2. EFFLUENT b. MAXIMUM 30 DAY VALUE (if available) 13,413 39,499 (2) MASS 1,056 MAXIMUM 729 90.1/32.3 90.2/32.3 2.06 CONCENTRATION 2,303 MINIMUM 6.5 782 62 42 VALUE VALUE VALUE MAXIMUM 7.3 a. MAXIMUM DAILY VALUE (2) MASS 16,229 89,451 10,782 2,735 3,173 92.0/33.3 91.0/32.8 2.9 (1) CONCENTRATION 1,075 4,942 186 156 MINIMUM 6.4 904 VALUE VALUE VALUE c. Total Organic Carbon a. Biochemical Oxygen Demand (BOD) b. Chemical Oxygen Demand (COD) 1. POLLUTANT d. Total Suspended Solids (TXX) e. Ammonia (as N) Temperature Temperature (winter) (DOC) f. Flow i. pH

Mark "X" in column 2-a for each pollutant you know or have reason to believe is present. Mark "X" in column 2-b for each pollutant you believe to be absent. If you mark column 2a for any pollutant which is limited either directly, or indirectly but expressly, in an effluent limitations guideline, you must provide the results of at least one analysis for that pollutant. For other pollutants for which you mark column 2a, you must provide quantitative data or an explanation of their presence in your discharge. Complete one table for each outfall. See the instructions for additional details and requirements. PART B-

	2. MA	2. MARK "X"			2. MARK "X" 3. EFFLUENT 4. UNITS	3. EFFLUENT				4. UNITS	S	5. INTA	5. INTAKE (optional)	
1. POLLUTANT AND		_	a. MAXIMUM DAILY VALUE	ILY VALUE	b. MAXIMUM 30 DAY (if available)	DAY VALUE	b. MAXIMUM 30 DAY VALUE c. LONG TERM AVRG. VALUE (if available)	VRG. VALUE				a. LONG TERM AVERAGE VALUE	WERAGE	
(if available)	PRESENT	ABSENT	(1) CONCENTRATION	(2) MASS	(1) CONCENTRATION		(2) MASS CONCENTRATION	(2) MASS	d. NO. OF ANALYSES	a. CONCENTRATION	b. MASS	(1) CONCENTRATION	(2) MASS	(2) MASS ANALYSES
a. Bromide (24959-67-9)	×		26.4	315					1	mg/L	lb/da			
b. Chlorine, Total Residual		×												
c. Color	×		200						1	color un				
d. Fecal Coliform		×												
e. Fluoride (16984-48-8)		×	QN						1	mg/L				
f. Nitrate-Nitrite (as N)		X	ND	ND			ON	QN	1	mg/L	1b/da			

EPA Form 3510-2C (8-90)

CONTINUE ON REVERSE

ITEM V-B CONTINUED FROM FRONT

	2. MAI	2. MARK "X"			m	3. EFFLUENT				STINIT A	TC	TINI 2	AKE (ontions	<
1. POLLUTANT AND		ď	a. MAXIMUM DAILY VALUE	AILY VALUE	b. MAXIMUM 30 DAY VALUE (if available)	DAY VALUE	c. LONG TERM AVRG. VALUE	VRG. VALUE				a. LONG TERM	NG TERM	
CAS NO. (if available)	BELIEVED	BELIEVED	0	(2) MASS	(1) CONCENTRATION	(2) MASS	(1) CONCENTRATION	(2) MASS	d. NO. OF ANALYSES	a. CONCENTRATION	b. MASS	(1) CONCENTRATION	ASS.	b. NO. OF ANALYSES
g. Nitrogen, Total Organic (as N)	X		206	2,984	105		100	1,570	196	mg/L	_			
h. Oil and Grease	×		29	369	8.8	151	11	171	102	mg/L	1b/da			
i. Phosphorus (as P), Total (7723-14-0)	X		24	453	8.8	150	6.8	107	196	mg/L	1b/da			
j. Radioactivity														
(1) Alpha, Total		×												
(2) Beta, Total		×												
(3) Radium, Total		X												
(4) Radium 226, Total		X												
k. Sulfate (as SO <sub>4</sub> ) (14808-79-8)	×		790	9,428					1	mg/L	lb/da			
I. Sulfide (as S)	×		6.6	118					1	mg/L	1b/da			
m. Sulfite (as SO <sub>3</sub> ) (14265-45-3)	X		85.5	1,020					П	mg/L	lb/da			
n. Surfactants		×	QN						1	mg/L				
o. Aluminum, Total (7429-90-5)	×		8.6	209			2.8	44	10	mg/L	lb/da			
p. Barium, Total (7440-39-3)	×		0.0078*	0.092					п	mg/L	1b/da			
q. Boron, Total (7440-42-8)	×		1.63	19.4					п	mg/L	1b/da			
r. Cobalt, Total (7440-48-4)		×	ND						1	mg/L				
s. Iron, Total (7439-89-6)	×		1.545	18.4					1	mg/L	lb/da			
t. Magnesium, Total (7439-95-4)	×		505	6,021					н	mg/L	lb/da			
u. Molybdenum, Total (7439-98-7)	×		0.0055*	0.066					н	mg/L	lb/da			
v. Manganese, Total (7439-96-5)	×		0.0241	0.288					1	mg/L	1b/da			
w. Tin, Total (7440-31-5)		×	ON						1	mg/L				
x. Titanium, Total (7440-32-6)	×		0.0032*	0.038					н	mg/L	lb/da			
EPA Form 3510-2C (8-90)	.2C (8-90)						PAGE V-2					5	CONTINUE ON BACK	0.00

OUTFALL NUMBER EPA I.D. NUMBER (copy from Item I of Form I) ASD 983 366 030

CONTINUED FROM PAGE 3 OF FORM 2-C

b. NO. OF ANALYSES PART C - If you are a primary industry and this outfall contains process wastewater, refer to Table 2c-2 in the instructions to determine which of the GC/MS fractions you must test for. Mark "X" in column 2-a for all such GC/MS fractions that apply to your industry and for ALL toxic metals, cyanides, and total phenols. If you are not required to mark column 2-a (secondary industries, nonprocess wastewater outfalls, and nonrequired GC/MS fractions), mark "X" in column 2-b for each pollutant you whow or have reason to believe is present. Mark "X" in column 2-c for each pollutant you believe is absent. If you mark column 2b for any pollutant, you must provide the results of at least one analysis for that pollutant. If you mark column 2b for any pollutant, you must provide the results of at least one analysis for that pollutant. If you mark column 2b for acrolein, acrylonitrile, 2.4 dinitrophenol, you must provide the results of at least one analysis for each of these pollutants which you know or have reason to believe that you discharge in concentrations of 100 ppb or greater. Otherwise, for pollutants for which you mark column 2b, you must either submit at least one analysis or briefly describe the reasons the pollutant is expected to be discharged. Note that there are 7 pages to this part, please review each carefully. Complete one table (all 7 pages) for each outfall. See instructions for b. NO. 5. INTAKE (optional) (2) MASS a. LONG TERM AVERAGE VALUE CONCENTRATION b. MASS lb/da 1b/da 1b/da 1b/da lb/da 1b/da lb/da 4. UNITS a. CONCENTRATION mg/L mg/L mg/L mg/L mg/L mg/L mg/L mg/L mg/I mg/L mg/L mg/L d. NO. OF ANALYSES Н LO 21 21 Н 2 N N H (2) MASS 0.14 0.002 0.073 0.11 c. LONG TERM AVRG. VALUE (if available) CONCENTRATION 0.00015 0.0070 0.0087 0.0047\* 0.012 b. MAXIMUM 30 DAY VALUE (2) MASS 3. EFFLUENT (if available) CONCENTRATION a. MAXIMUM DAILY VALUE 0.0068 (2) MASS 1.11 0.44 0.18 0.39 0.15 0.70 (1) CONCENTRATION 0.00028 0.0063\* 0.0932 0.0075 0.0588 0.018 0.016 R B N B R BELIEVED BELIEVED PRESENT ABSENT additional details and requirements. METALS, CYANIDE, AND TOTAL PHENOLS 2. MARK "X" a. TESTING REQUIRED 1M. Antimony, Total 4M. Cadmium, Total 3M. Beryllium, Total 1. POLLUTANT CAS NUMBER 8M. Mercury, Total 2M. Arsenic, Total 11M. Silver, Total Total (7440-28-0) 6M. Copper, Total (7440-50-8) 5M. Chromium, Total (7440-47-3) Total (7782-49-2) (if available) 9M. Nickel, Total 13M. Zinc, Total 7M. Lead, Total 12M. Thallium 10M. Selenium (7440-22-4)(7439-92-1) (7440-02-0) (7440-36-0)(7440 - 38 - 2)(7440-41-7) (7440-43-9)7439-97-6)

Analyzed during February 2016 Priority Pollutant Scan.

DESCRIBE RESULTS

EPA Form 3510-2C (8-90)

Dioxin (1764-01-6)

2,3,7,8-Tetra-chlorodibenzo-P-

DIOXIN Total

PAGE V-3

Result was non-detect (reported to BPA)

1b/day

mg/L

1.04 0.024 3.6

0.0629

0.002\* 0.301

14M. Cyanide, Total (57-12-5)

(7440-66-6)

15M. Phenols,

lb/da 1b/da

mg/L

mg/L

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CONTINOED LYON THE	MADK "Y"				2 EEEL LIENT				OTHER.			4
1. POLLUTANT	Z. MANA				b. MAXIMUM 30 DAY VALUE	O.	WRG.		1	0	a. LONG TERM	191)
CAS NUMBER TE	a. b. TESTING BELIEVED REQUIRED PRESENT	C. BELIEVED	a. MAXIMUM DAILY VALUE (1) CONCENTRATION (2) MASS	(2) MASS	(if available) (1) CONCENTRATION (2) MASS	(1) (2) MASS	d. N d. N	d. NO. OF a. CC ANALYSES TRA	a. CONCENTRATION	b. MASS	AVERAGE VALUE (1) (2) MASS	b. NO. OF
GC/MS FRACTION - VOLATILE COMPOUNDS	OLATILE COMPO	SUNDS					200			7		
1V. Accrolein (107-02-8)		×	ND					1 mg	mg/L			
2V. Acrylonitrile (107-13-1)		×	UD					1 mc	mg/L			
3V. Benzene (71-43-2)	×		0.00034*	0.0041				1 m	mg/L	lb/da		
4V. Bis (Chloro- methyl) Ether (542-88-1)		X	QN					1 mc	mg/L			
5V. Bromoform (75-25-2)		×	OND					1 mc	mg/L			
6V. Carbon Tetrachloride (56-23-5)		×	ON					1 mc	mg/L			
7V. Chlorobenzene (108-90-7)		×	ON					1 mc	mg/L			
8V. Chlorodi- bromomethane (124-48-1)		X	QN					1 mc	mg/L			
9V. Chloroethane (75-00-3)		×	QN					1 mc	mg/L			
10V. 2-Chloro- ethylvinyl Ether (110-75-8)		X	QN					1 mc	mg/L			
11V. Chloroform (67-66-3)	×		*50000.0	9000.0				1 mc	mg/L	lb/da		
12V. Dichloro- bromomethane (75-27-4)		X	ON					- T	mg/L			
13V. Dichloro- difluoromethane (75-71-8)		×	QN					1 mc	mg/L			
14V. 1,1-Dichloro- ethane (75-34-3)		×	QN					1 mc	mg/L			
15V. 1,2-Dichloro- ethane (107-06-2)		×	QN					1 mg	mg/L			
16V. 1,1-Dichloro- ethylene (75-35-4)		×	ON					1 mg	mg/L			
17V. 1,2-Dichloro- propane (78-87-5)	×		0.0001*	0.0012				1 mg	mg/L	lb/da		
18V. 1,3-Dichloro- propylene (542-75-6)		X	ND					1 mc	mg/L			-
19V. Ethylbenzene (100-41-4)	×		0.00017*	0.002				1 mg	mg/L	1b/da		
20V. Methyl Bromide (74-83-9)		×	ON					1 mg	mg/L			
21V. Methyl Chloride (74-87-3)		×	ND				4122	1 mg	mg/L			
EPA Form 3510-2C (8-90)	(06				PAGE V-4	E V-4					CONTINUE ON PAGE V-5	N PAGE V-5

CONTINUED FROM PAGE V-4

Service of the servic	CA	2. MARK "X"				3. EFFLUENT			4. UNITS	IITS	5. INTAKE (optional)	
1. POLLUTANT AND	ej	Ġ	ú	a. MAXIMUM DAILY VALUE	AILY VALUE	b. MAXIMUM 30 DAY VALUE (if available)	c. LONG TERM AVRG. VALUE (if available)				a. LONG TERM AVERAGE VALUE	
(if available)	REQUIRED	BELIEVED	BELIEVED	(1) CONCENTRATION	(2) MASS	CONCENT	8	d. NO. OF ANALYSES	a. CONCENTRATION	b. MASS	ASS	b. NO. OF ANALYSES
GC/MS FRACTION - VOLATILE COMPOUNDS (continued)	N - VOLATIL	E COMPOU	UNDS (cont	(panui,			1				b	
22V. Methylene Chloride (75-09-2)		×		0.00025*	0.003			1	mg/L	lb/da		
23V. 1,1,2,2- Tetrachloroethane (79-34-5)			X	QN				1	T/Sm			
24V. Tetrachloro- ethylene (127-18-4)			×	QN				1	mg/L			
25V. Toluene (108-88-3)		X		0.00041*	0.0049			1	mg/L	lb/da		
26V. 1,2-Trans- Dichloroethylene (156-60-5)			X	ND				1	mg/L			
27V. 1,1,1-Trichloro- ethane (71-55-6)			X	ON				1	mg/L			
28V. 1,1,2-Trichloro- ethane (79-00-5)			X	ON				1	mg/L			
29V Trichloro- ethylene (79-01-6)			×	ND				1	mg/L			
30V. Trichloro- fluoromethane (75-69-4)			X	UND				1	mg/L			
31V. Vinyl Chloride (75-01-4)			×	ON				1	mg/L			
GC/MS FRACTION - ACID COMPOUNDS	1 - ACID CO.	MPOUNDS										
1A. 2-Chlorophenol (95-57-8)			×	ON				1	mg/L			
2A. 2,4-Dichloro- phenol (120-83-2)			×	ND				1	mg/L			
3A, 2,4-Dimethyl- phenol (105-67-9)			×	ON				1	mg/L			
4A. 4,6-Dinitro-O- Cresol (534-52-1)			×	QN				1	mg/L			
5A. 2,4-Dinitro- phenol (51-28-5)			X	ND				П	mg/L			
6A. 2-Nitrophenol (88-75-5)			×	ON				1	mg/L			
7A. 4-Nitrophenol (100-02-7)			×	ND				1	mg/L			
8A. P-Chloro-M- Cresol (59-50-7)			×	ND				Т	mg/L			
9A. Pentachloro- phenol (87-86-5)			×	QN				1	mg/L			
10A. Phenol (108-95-2)		×		0.21**	2.51			Т	mg/L	lb/da		
11A. 2,4,6-Trichloro-			X	ND				П	mg/L			

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CONTINUED TROM THE TROM	0	2 MARK "X"			3 FFEI LIENT			A LIMITS	ITC	S INTAKE / American	Venez
1. POLLUTANT	i	4		AND MINISTER	b. MAXIMUM	c. LONG TERM AVRG.		ř	2	a. LONG TERM	onar
BER	TESTING B	BELIEVED E	BELIEVED ABSENT		_	(1) (2) MASS	d. NO. OF SS ANALYSES	a. CONCENTRATION	b. MASS	CONCENTRATION (2) MASS	b. NO. OF SS ANALYSES
GC/MS FRACTION - BASE/NEUTRAL COMPOUNDS	- BASE/NEU	JTRAL CON	MPOUND	S	ΙI						
1B. Acenaphthene (83-32-9)			×	ND			1	mg/L			
2B. Acenaphtylene (208-96-8)			×	CIN			1	mg/L			
3B. Anthracene (120-12-7)			X	CN			-1	mg/L			
4B. Benzidine (92-87-5)			X	QN			П	mg/L			
5B. Benzo (a) Anthracene (56-55-3)			×	DN			п	mg/L			
6B. Benzo ( <i>d</i> ) Pyrene (50-32-8)			X	CN			1	mg/L			
7B. 3,4-Benzo- fluoranthene (205-99-2)			×	QN			П	mg/L			
8B. Benzo (ghr) Perylene (191-24-2)			X	QN CN			П	mg/L			
9B. Benzo (k) Fluoranthene (207-08-9)			×	CIN			н	mg/L			
10B. Bis (2-Chloro- ethoxy) Methane (111-91-1)			X	ND			н	mg/L			
11B. Bis (2-C'hloro- ethyl) Ether (111-44-4)			×	QN			н	mg/L			
12B. Bis (2- ('hloroisopropyi) Ether (102-80-1)			×	QN			1	mg/L			
13B. Bis (2-Ethyl- hexyl) Phthalate (117-81-7)		X		0.11** 1.31	1		н	mg/L	lb/da		
14B. 4-Bromophenyl Phenyl Ether (101-55-3)			×	QN			Н	mg/L			
15B. Butyl Benzyl Phthalate (85-68-7)			×	ON			1	mg/L			
16B. 2-Chloro- naphthalene (91-58-7)			×	QN			н	mg/L			
17B. 4-Chloro- phenyl Phenyl Ether (7005-72-3)			×	CN			п	mg/L			
18B. Chrysene (218-01-9)			×	QN			1	mg/L			
19B. Dibenzo (a.h) Anthracene (53-70-3)			×	QN			1	mg/L			
20B. 1,2-Dichloro- benzene (95-50-1)			×	ND			1	mg/L			
21B. 1,3-Di-chloro- benzene (541-73-1)			X	ND			1	T/6m			
EPA Form 3510-2C (8-90)	(8-90)				PAGE V-6	. V-6				CONTINUE	CONTINUE ON PAGE V-7

CONTINUED FROM PAGE V-6

ON CONTRACTOR	2. M	2. MARK "X"			3 FFFI UENT			STINIT A	TS	5 INTAKE (ontlone)	V
	ro'	۵		a. MAXIMUM DAILY VALUE	b. MAXIMUM	c. LONG TERM AVRG. VALUE (if available)				a. LONG TERM AVERAGE VALUE	
(if available)	TESTING BE REQUIRED PR	NED ENT	BELIEVED	(1) CONCENTRATION (2) MASS	-	(1) CONCENTRATION (2) MASS	d. NO. OF ANALYSES	a. CONCENTRATION	b. MASS	(1) CONCENTRATION (2) MASS	D. NO. OF ANALYSES
GC/MS FRACTION - BASE/NEUTRAL COMPOUNDS (continued)	- BASE/NEU	TRAL COMF	POUNDS	S (continued)							
22B. 1,4-Dichloro- benzene (106-46-7)			X	ND			1	mg/L			
23B. 3,3-Dichloro- benzidine (91-94-1)			X	CIN			1	mg/L			
24B. Diethyl Phthalate (84-66-2)		, \	X	CIN			1	mg/L			
25B. Dimethyl Phthalate (131 -11-3)			X	CN			1	mg/L			
26B. Di-N-Butyl Phthalate (84-74-2)			X	CIN			1	mg/L			
27B. 2,4-Dinitro- toluene (121-14-2)			X	ON			1	mg/L			
28B. 2,6-Dinitro- toluene (606-20-2)			X	CIN			Н	mg/L			
29B. Di-N-Octyl Phthalate (117-84-0)			X	CN			н	mg/L			
30B. 1,2-Diphenyl- hydrazine (as Azo- benzene) (122-66-7)			X	QN			П	mg/L			
31B. Fluoranthene (206-44-0)			X	CIN			1	mg/L			
32B. Fluorene (86-73-7)		/ \	X	QIN			1	mg/L			
33B. Hexachloro- benzene (118-74-1)		× .	X	CIN			1	mg/L			
34B. Hexachloro- butadiene (87-68-3)			X	CN			1	mg/L			
35B. Hexachloro- cyclopentadiene (77-47-4)		/\	X	CN			1	mg/L			
36B Hexachloro- ethane (67-72-1)			X	ND			П	mg/L			
37B. Indeno (1,2,3-cd) Pyrene (193-39-5)			X	ND			Н	mg/L			
38B. Isophorone (78-59-1)			X	QN			1	mg/L			
39B. Naphthalene (91-20-3)		/ \	X	ND			н	mg/L			
40B. Nitrobenzene (98-95-3)		/\	X	ON			1	mg/L			
41B. N-Nitro- sodimethylamine (62-75-9)		/ \	X	ND			П	mg/L			
42B. N-Nitrosodi- N-Propylamine (621-64-7)		/\	X	ND			1	mg/L			
EPA Form 3510-2C (8-90)	3-90)				PAGE V-7	V-7				CONTINUE ON REVERSE	N REVERSE

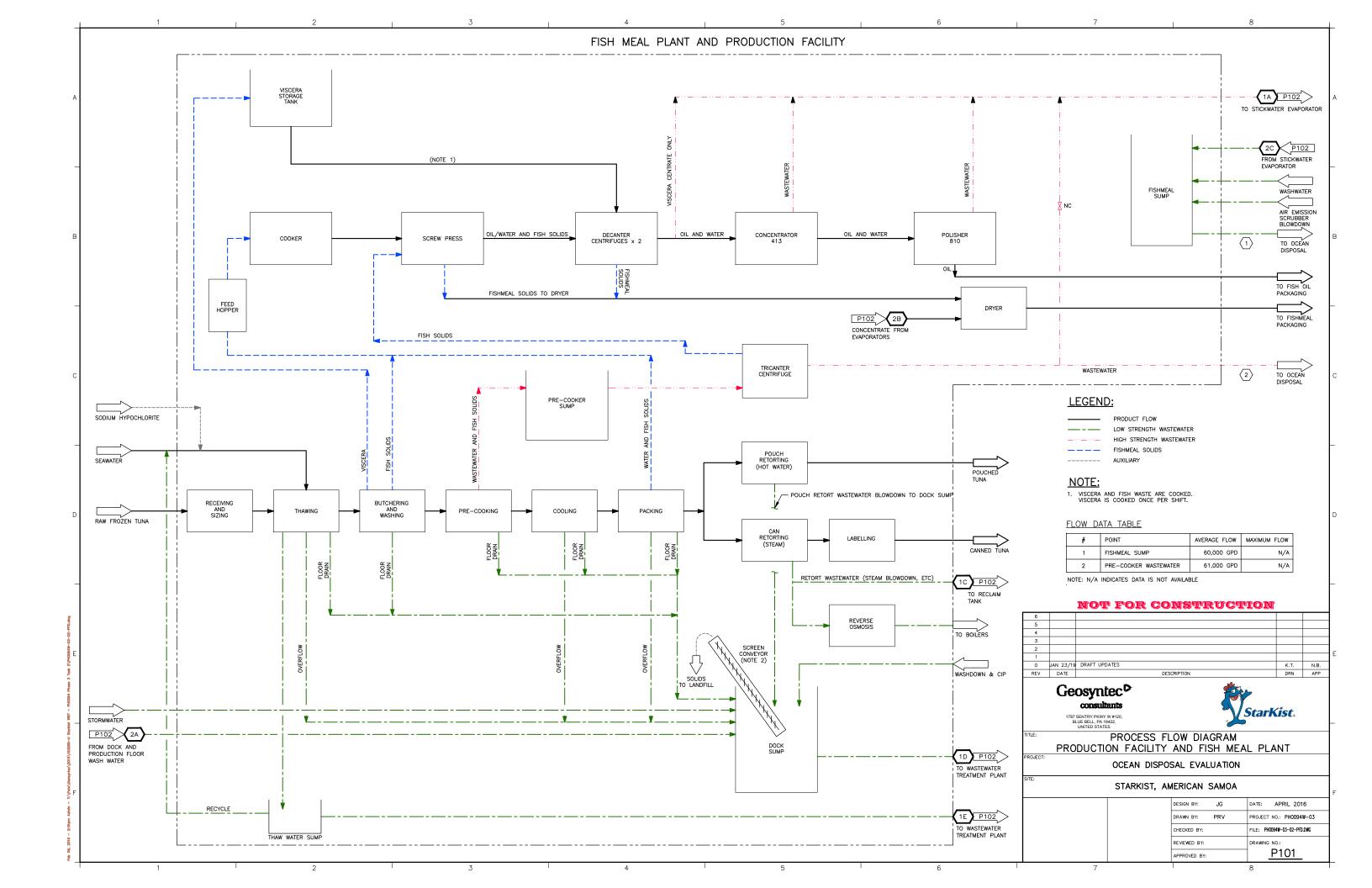
CONTINUED FROM THE FRONT

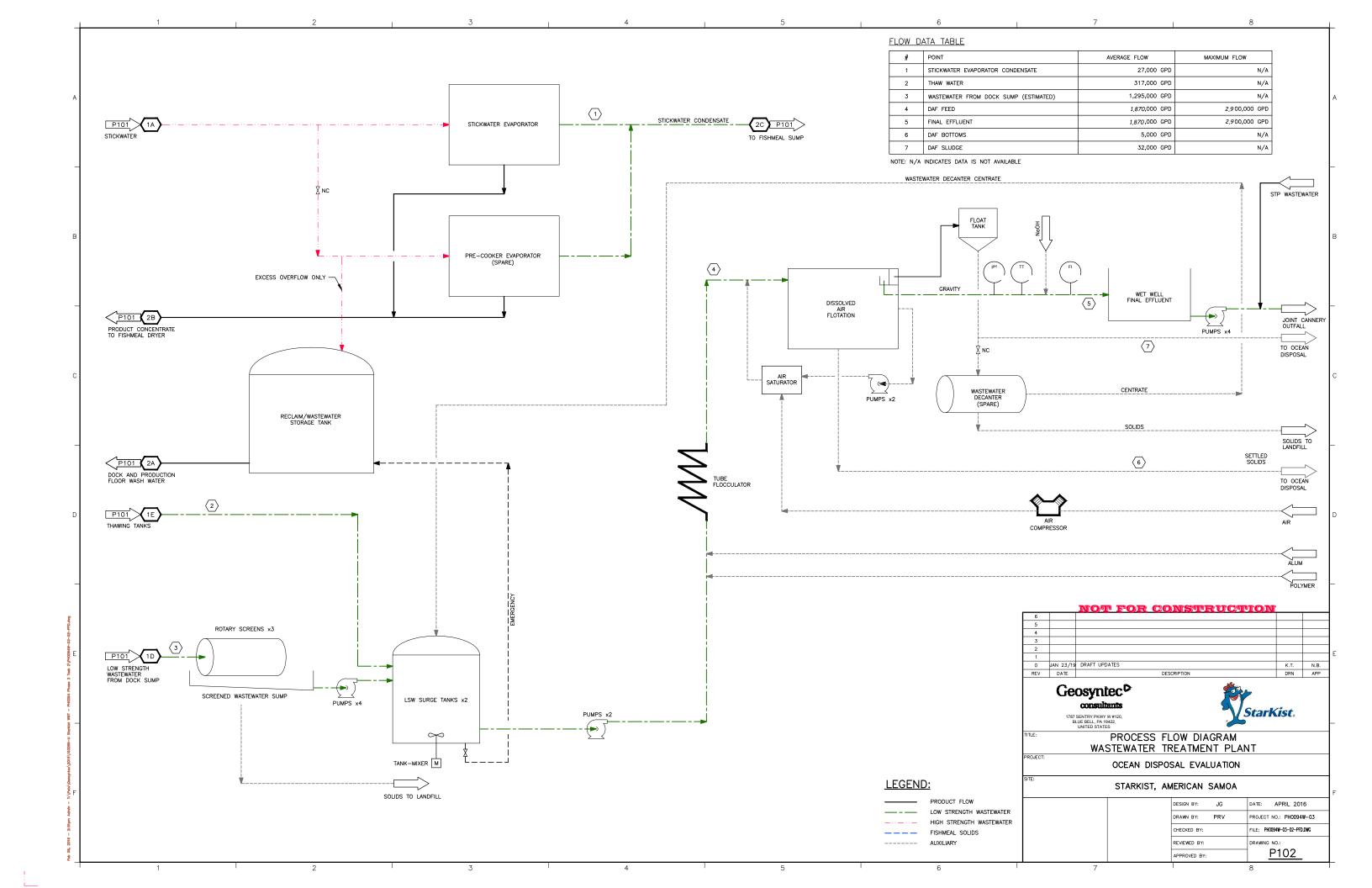
CONTINOED TROM THE TROM	2	2. MARK "X"			3 FFFI UFNT			A LINITS	ITC	JINI 3	S INTAKE (ontional)	
1. POLLUTANT					b. MAXIMUM	c. LONG TERM AVRG.		-		a. LONG T	ERM	
CAS NUMBER (If available)	a. b. TESTING BELIEVED REQUIRED PRESENT	b. BELIEVED PRESENT	BELIEVED ABSENT	a. MAXIMUM DAILY VALU	ш "	2	d. NO. OF	a. CONCENTRATION	b MASS	AVERAGE VALUE	ALUE	- b. NO. OF
GC/MS FRACTION - BASE/NEUTRAL COMPOUNDS (continued)	- BASE/NE	UTRAL CO	MPOUNDS							CONCENTRATION	(2) MASS	
43B. N-Nitro- sodiphenylamine (86-30-6)			X	QN			Н	mg/L				
44B. Phenanthrene (85-01-8)			X	CIN			1	mg/L				
45B. Pyrene (129-00-0)			X	QN			1	mg/L				
46B. 1,2,4-Tri- chlorobenzene (120-82-1)			X	QN O			1	mg/L				
GC/MS FRACTION - PESTICIDES	I - PESTICIE	DES										
1P. Aldrin (309-00-2)			X	ON			1	mg/L				
2P. α-BHC (319-84-6)			×	QN			1	mg/L				
3P. β-BHC (319-85-7)			×	QN			1	mg/L				
4P. y-BHC (58-89-9)			×	ON			1	mg/L				
5P. 8-BHC (319-86-8)			×	QN			П	mg/L				
6P. Chlordane (57-74-9)			×	QN			Н	mg/L				
7P. 4,4'-DDT (50-29-3)			×	ON			1	mg/L				
8P. 4,4'-DDE (72-55-9)			X	UD			1	mg/L				
9P. 4,4'-DDD (72-54-8)			×	UD			Т	mg/L				
10P. Dieldrin (60-57-1)			×	CIN			п	mg/L				
11P. α-Enosulfan (115-29-7)			×	ON			г	mg/L				
12P. β-Endosulfan (115-29-7)			X	UD			1	mg/L				
13P. Endosulfan Sulfate (1031-07-8)			X	UD			1	mg/L				
14P. Endrin (72-20-8)			×	ND			1	mg/L				
15P. Endrin Aldehyde (7421-93-4)			X	ND			1	mg/L				
16P. Heptachlor (76-44-8)			×	ND			1	mg/L				
EPA Form 3510-2C (8-90)	(06-8)				PAGE V-8	V-8				100	CONTINUE ON PAGE V-9	PAGE V-9

		optional)		(2) MASS ANALYSES										
		5. INTAKE (optional)	a. LONG TERM AVERAGE VALUE	(1) CONCENTRATION (2) M										
		TS		b. MASS										
		4. UNITS		a. CONCENTRATION		mg/L	mg/L	T/6m	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L
Г				d. NO. OF ANALYSES		1	П	н	1	1	1	П	П	-
BER	001		M AVRG. ailable)	(2) MASS										
OUTFALL NUMBER	0		c. LONG TERM AVRG. VALUE (if available)	(1) CONCENTRATION										
		3. EFFLUENT	AY VALUE	(2) MASS										
R (copy from Item 1 o	983 366 030	3. E	b. MAXIMUM 30 DAY VALUE (if available)	(1) CONCENTRATION										
.D. NUMBER	ASD 9		LY VALUE	ON (2) MASS										
EPA I.D. NUMBER (copy from I of Form I)			a. MAXIMUM DAILY VALUE	(1) CONCENTRATION		QN	ON	QN	QN	MD	ON	ON	ON	ON
					(pan	X	×	×	×	×	×	×	×	×
		2. MARK "X"	b.	BELIEVED BELIEVED PRESENT ABSENT	DES (contin									
	M PAGE V-8	2		TESTING	- PESTICIL									
	CONTINUED FROM PAGE V-8		1. POLLUTANT AND	CAS NUMBER (if available)	GC/MS FRACTION - PESTICIDES (continued)	17P. Heptachlor Epoxide (1024-57-3)	18P. PCB-1242 (53469-21-9)	19P, PCB-1254 (11097-69-1)	20P. PCB-1221 (11104-28-2)	21P. PCB-1232 (11141-16-5)	22P. PCB-1248 (12672-29-6)	23P. PCB-1260 (11096-82-5)	24P. PCB-1016 (12674-11-2)	25P. Toxaphene (8001-35-2)

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# **ATTACHMENT A - NPDES Application Form 2C Supplemental Materials**

# Section II.B.2 (Form 2C) - Operations Description

#### 1. Product Flow

Frozen raw whole tuna is received and unloaded at the Facility and stored in freezers. The tuna is sorted for size and species by hand and by automated sorting equipment. Frozen tuna is defrosted in bins under a cascading sodium hypochlorite treated seawater stream prior to processing. Thawed tuna is transferred to a butchering area where the tuna is washed, the viscera are removed and the tuna is evaluated for quality. Butchered tuna is loaded onto racks, injected with broth, and carted into one of 11 steam pre-cookers. The pre-cooked tuna is cooled and manually transferred to the packaging area. The pre-cooked tuna is then cleaned, trimmed, deboned, and packaged into cans or foil and polyethylene plastic pouches. Cans of tuna are sealed, loaded into baskets, and processed in steam retort units that are pressurized with high temperature steam to sterilize the cans. Pouches of tuna are processed in pouch retort units that utilize heated water. Finished cans of tuna are labeled and marked with production information. The cans are then packaged into boxes and the boxes are labeled with various production information. Pouches arrive at the Facility prelabeled, but the sealed pouches are marked with product information and then packaged into boxes. The finished products are then palletized and stored awaiting shipment.

# 2. Fishmeal Processing

Fish scraps from the packing room are transferred to the Fishmeal Plant via a screw auger. The fish solids from the packing room are then cooked and pressed to separate liquid from the fish solids. The solids continue through a drying process and then to packaging, while the fishmeal processing screw press water ("press water" or "stickwater") is directed to a series of oil separaters to maximize the capture of fishoil and fishmeal. Stickwater is then transferred to a dedicated evaporator where waste heat from the dryer is applied to heat the stickwater and evaporate water, concentrating the remaining fish solids. The concentrated stickwater stream is then combined with the fish solids, and the precooker evaporator concentrate, and dried through the dryer. Recovered oil is packaged as fish oil.

Fish scraps from the butchering and washing process are referred to as viscera and are pumped to the viscera tank in Fishmeal Plant via a viscera solids pump or are transported in scows. The viscera are stored in a dedicated tank and cooked with steam once per shift, pumped to a grinder, and subsequently pumped to one of two fishmeal decanters. The accumulated liquid in the viscera tank is pumped to the stickwater evaporator as described above. Please refer to Drawing P101 and Drawing P102.

#### 3. Wastewater Flow

Wastewater from the Facility is primarily generated during normal production and sanitation operations from the pre-cooker, the fishmeal processing area, thawing, butchering, cooling, packing, retort, and dock area wash down activities. All sanitary waste from the Facility is conveyed to the Utulei wastewater treatment plant operated by the American Samoa Power Authority (ASPA). Stormwater from the dock, alleys, retort area roof and wastewater treatment areas is treated, as described in this Attachment (Section II.B.3). The Facility operates five or six days per week, with carry-over to the sixth day for sanitation and cleaning activities. The wastewater is separated into two categories: high strength wastewater (HSW) and low strength wastewater (LSW). An overview of the production processes that result in the generation of wastewater at the Facility is provided on Drawing P101.

HSW from the pre-cookers is generated from the contact of steam with the cooking fish and from the release of liquids as the fish is cooked. This wastewater is directed to the pre-cooker sump, which is adjacent to the pre-cookers. The wastewater is then transferred to a three-phase centrifuge (tricanter centrifuge) for preliminary removal of solids and fishoil (process code 5-D). Tricanter centrifuge effluent (centrate) is then pumped to the pre-cooker evaporator to capture additional fishmeal solids. Fishmeal plant HSW is described in Section II.B.3.

The stickwater and pre-cooker evaporators collectively generate two different LSW streams, both of which are directed to the wastewater treatment system: condensate wastewater and clean-in-place (CIP) wastewater. The characteristics of the condensate wastewater have low concentrations of total suspended solids (TSS), oil and grease (O&G), total phosphorus (TP) and organic nitrogen. It has been observed that the condensate wastewater contains a moderate concentration of ammonia. The evaporator CIP process uses 5% sodium hydroxide solution to periodically remove accumulated O&G and fish solids from the internal cavities of the evaporators. From information provided by the equipment vendor, StarKist anticipates that the CIP process will be required approximately once per week and will generate 350 gallons of the 5% solution, which will be discharged to the facility's wastewater treatment system. The chemicals in the CIP wastewater will be "spent" and final chemical rinses will be held in the system and used as the first rinses on the next CIP cycle. The condensate and CIP wastewater will be discharged to the wastewater treatment system.

Wastewater is also generated by two new air emissions scrubbers, which have been installed to address odors from the fishmeal processing equipment, and by washdown. The air emissions scrubbers may use 35% sulfuric acid, 50% sodium hydroxide and 12.5% sodium hypochlorite in two separate stages to first remove ammonia odors, and then remove odors associated with volatile organic compounds and hydrogen sulfide. The actual chemical quantities required in each scrubber are minimal and approximately 12,000 gallons per day of scrubber wastewater is generated at a pH ranging from 8 to 9<sup>1</sup>. The scrubber wastewater is discharged to the fishmeal sump and then the

<sup>&</sup>lt;sup>1</sup> Currently, StarKist has not been adding chemicals to the scrubbers as odors have not been detected through regular monitoring of the scrubber exhaust.

facility's wastewater treatment system via the dock sump. A fishmeal sump is used to collect washdown, steam condensate, and a portion of evaporator condensate from all areas of the Fishmeal Plant, and to transfer the wastewater to the LSW treatment system via the dock sump.

LSW from the butchering and cooling area is primarily generated from rinsing processing equipment, plus sanitation operations. Wastewater from this area flows by gravity from local drains to the dock sump. Wastewater is generated from the packing area during both production and sanitation activities and is transferred by gravity through floor drains and in-line strainer baskets to the dock sump. Floor washing and general housekeeping wastewater is also directed to the wastewater treatment system via the dock sump.

LSW generated from the can retort equipment is generally comprised of once through cooling water. The cooling water is supplied by ASPA and treated with sodium hypochlorite to a residual chlorine concentration of 1 mg/L before entering the retorts. The can retorts are filled with cooling water at the end of each cycle to reduce the temperature of the cans prior to removal and handling. The cooling water is pumped to a cooling water reclaim tank to reduce its temperature, and then a portion is treated via reverse osmosis and reused as boiler feed water. Reclaimed water that is not reused flows to a pumping system located near the wastewater treatment system, which feeds dock washing, floor washing, and other non-contact uses in the main production facility. Unused reclaim water flows to the screen effluent sump where it joins the screened wastewater from the dock sump. Cooling water from the pouch retort area is internally recycled through cooling towers and the cooling tower blowdown is discharged to the dock sump.

Seawater used to thaw frozen fish is collected in a collection sump and recirculated for the entire thawing cycle. The thawing water is treated by sodium hypochlorite as it is recirculated to maintain a residual chlorine concentration ranging from 2 to 5 ppm to prevent microbe growth (process code 2-F). Once a thawing cycle is complete, wastewater generated by the thawing process is pumped directly to the LSW surge tanks. A portion of the thaw water also flows to the east dock trench which then discharges to the dock sump. Please refer to Drawing P101 and Drawing P102. Estimations of average flow from Facility operations are included in Drawing P102 and Section II.B.3 (below).

# Section II.B.3 (Form 2C) - Wastewater Treatment Description

## 1. High Strength Wastewater (HSW) Treatment System

HSW is generated by two primary operations: fish pre-cooking and fishmeal solids processing. HSW represents approximately 4.5% of the total wastewater volume generated by the Facility on a daily basis, of which the stickwater contributes 1.5% and the pre-cooker contributes the remaining 3.1%. The estimated average total daily wastewater flow generated by the Facility is 2,000,000 gallons per day (gpd), of which approximately 90,500 gpd is considered HSW.

As described in Section II.B.2, HSW is processed through two process evaporators to reduce the volume, and the evaporator concentrate is processed with fishmeal solids through the dryer.

Wastewater discharged to the treatment system from the fishmeal and pre-cooker areas now includes evaporator condensate and scrubber blowdown. Both wastewater streams from the evaporator systems are discharged to the wastewater treatment system via the dock sump. The historical HSW treatment system has been decommissioned.

## 2. Low Strength Wastewater (LSW) Wastewater Treatment System

Wastewater generated from all other sources at the Facility, including production operations, washing and rinsing of equipment, sanitation processes, and impacted stormwater from alleys, rooftops, and dock areas, is considered LSW, and combines with the evaporator condensate and scrubber blowdown in the Dock Sump as described in Section II.B.2.

Wastewater leaving the dock sump represents approximately 60% of the total wastewater volume generated by the Facility on a daily basis. The estimated average total daily wastewater flow generated by the Facility is 2,000,000 gpd<sup>2</sup>, of which an estimated 1,295,000 gpd is collected and pumped from the dock sump, including rainfall.

The average rainfall is estimated to result in approximately 24,000 gpd of stormwater runoff collected in the dock sump, based on climate data for the American Samoa region from a dataset spanning 22 years (1990 to 2012) and a total exposed facility area draining to the wastewater treatment plant (including the wastewater treatment area) of approximately 142,000 square feet (ft²), calculated from dimensions taken from Drawing M001 (also shown in the EPA Multi Sector General Permit Stormwater Pollution Prevention Plan [SWPPP] for StarKist [Map #2]). Peak rainfall is estimated to contribute approximately 947,000 gallons in one day, based on climate data from the last 15 years.

Rainfall that collects on the dock, impacted rooftops, alleys, and wastewater treatment areas is directed to the dock sump for treatment through a dissolved air flotation (DAF) system further described below. The following areas of the facility potentially contribute stormwater that is treated by the facility: roof drains from the boiler stacks and fishmeal area, docks (where fish handling and unloading occurs), and alleys (where sanitation chemicals are stored, under cover, in addition to food ingredients such as olive oil and vegetable oil).

The majority of the wastewater generated at the site accumulates in the dock sump from various areas and generation points as noted on drawings P101 and P102. Wastewater from the dock sump is screened via an automated screening system (process code 1-T) and is then pumped to three rotary screens operating in parallel for additional coarse solids removal (process code 1-T). The wastewater then gravity drains into the screen effluent sump, where it is pumped to the wastewater surge tanks. The overflow from the reclaim water tank also discharges to the screen effluent sump, where it is combined with the wastewater and transferred to the LSW surge tanks. The surge tanks also receive spent thaw water. The surge tanks are hydraulically connected to the reclaim water

<sup>&</sup>lt;sup>2</sup> The anticipated maximum daily wastewater flow generated by the facility is 3,000,000 gpd, based on the estimated maximum daily flow corresponding to the maximum daily production anticipated for the next permit term.

tank to provide a total working volume of approximately 137,000 gallons. The surge tanks are used to dampen the hydraulic surges from the processing facility and maintain a more consistent flow through the wastewater treatment system. The surge tanks will be equipped with mixers in 2019 to keep solids suspended. Solids removed from the surge tanks and rotary screens are sent to the local landfill for disposal.

Wastewater is pumped from the surge tanks to the DAF unit prior to final discharge (process code 1-H). The DAF unit is the primary wastewater treatment process in the wastewater treatment train and removes TP, total nitrogen (TN), TSS, and O&G from the wastewater stream in advance of discharge via the outfall. The DAF unit has the following dimensions:

Depth: 20 feet (ft)Diameter: 45 ft

• Operating volume: 237,000 gallons

• Capacity: approximately 2,600,000 gpd<sup>3</sup>

• Average surface loading rate: approximately 0.87 gpm per square foot (gpm/ft²)

• Solids loading rate: approximately 1.75 pound per hour per square foot (lb/hr/ft²)

From the surge and reserve tanks, the raw wastewater is pumped to the pipe flocculator. Alum (aluminum sulfate) coagulant is injected into the wastewater where it enters the pipe flocculator, and polymer flocculant is injected further downstream inside the flocculator.

Immediately downstream of the flocculator, the wastewater is blended with a side stream of recirculated, clarified water from the DAF tank. This recirculated stream is injected with compressed air following discharge from the DAF tank and then blended into the flocculated wastewater stream via two DAF recirculation pumps installed in parallel (duty and standby).

The alum acts to coagulate wastewater particulates by neutralizing ionic charges, which causes flocculation and precipitation of dissolved phosphorus (process codes 1-G, 2-C, and 2-D). The polymer added promotes the formation of larger floc by forming long polymer chains around smaller particulates to improve capture across the DAF system (process code 1-G). The dissolved air introduced through the recirculation of final effluent is released once the wastewater reaches the atmosphere, generating bubbles which attach to solids and float them to the surface. Floating solids are skimmed from the top of the DAF tank and stored in a DAF float tank (process code 1-H). From the DAF float tank, the solids slurry is processed through a wastewater decanter, with polymer addition, to further separate solids from liquid (process code 5-D). Separated and dewatered solids are sent to the local landfill, while the centrate is returned to the DAF center well for further treatment.

<sup>&</sup>lt;sup>3</sup> The current capacity of the wastewater treatment system infrastructure is not adequate to treat the anticipated maximum daily flow requested in this permit application. However, the infrastructure will be upgraded as needed to provide the necessary capacity during the next permit term.

Wastewater enters the DAF system in a central well and spreads out radially to the outer edge of the unit, where it passes under a scum baffle and over an effluent weir into the effluent launder. From here, treated DAF effluent flows through a Parshall flume where an ultrasonic level sensor continuously measures the final effluent flow rate and a pH sensor continuously monitors the pH for compliance. Sodium hydroxide (NaOH) is metered in as needed to adjust the final effluent pH to achieve compliance with the effective NPDES permit limits (process code 2-K). Finally, effluent wastewater flows by gravity to the effluent wet well, from which it is pumped into the discharge pipeline and combined with final effluent from Samoa Tuna Processors, Inc. (STP) prior to discharge through the Joint Cannery Outfall (JCO).

# 3. Facility Wastewater Streams to Ocean Disposal

Historically, the ocean disposal program collected high strength wastewater streams from the Facility in a 300,000 gallon storage tank, and periodically disposed of the material at a permitted disposal location approximately 5 miles off-shore. StarKist is currently in the process of reinstating the ocean disposal program for several HSW sources at the Facility. The HSW considered for ocean disposal include:

- DAF Sludge;
- pre-cooker wastewater;
- evaporator condensate; and
- fishmeal sump.

Resuming ocean disposal of a portion of the HSW will reduce the loads discharged through the JCO to Pago Pago Harbor. A wastewater sampling event to quantify the pollutant loading from the wastewater streams that are being considered for ocean disposal was completed in November 2018. The data collected during the event for each of the ocean disposal streams were used to estimate the impact on the final effluent once ocean disposal is reinstated.

## Section V.A-C (Form 2C) - Effluent Characteristics

Because ocean disposal of a portion of the HSW has not yet resumed, measured effluent water quality data representing these conditions are not available. The final effluent characteristics presented in Form 2C were instead estimated based on the impact of disposing DAF sludge, precooker wastewater, evaporator condensate, and fishmeal sump wastewater on the final effluent. The wastewater effluent quality used to calculate the estimated wastewater effluent quality included all sampling results that are considered representative of StarKist's effluent water quality at the discharge monitoring point from April through December 2018. In mid-March 2018 a number of minor treatment system improvements were implemented including, relocation of the wastewater decanter centrate to the surge tank, increased viscera processing, fishmeal pumping configurations, and increased training and focus on spill prevention. These changes resulted in improved final effluent wastewater quality which was then maintained by the Facility for the rest of the year; therefore, wastewater data collected from April to December 2018 represents the current operating conditions. The data includes:

- final wastewater effluent data representing samples that are analyzed on-site and reported in the Discharge Monitoring Reports (DMRs);
- splits of these effluent samples that are analyzed by TestAmerica;
- effluent samples collected for the semi-annual JCO effluent testing reports; and
- samples collected for the Priority Pollutant Scan (PPS) analysis.

For days where more than one sample was collected and analyzed for a constituent (including split and duplicate samples), reported concentrations for all samples were averaged to compute an average daily concentration. The flow measured and presented in the DMR for the given day was then used to compute an average daily mass load.

The maximum daily loads were estimated by subtracting the estimated reduction in pollutant loading as a result of sending HSW to ocean disposal from the maximum loading of pollutants observed in the final effluent from April to December 2018. The maximum concentration of pollutants was estimated by calculating the maximum observed concentration of pollutants from April to December 2018, calculating the load of pollutants using the maximum observed flow from April to December 2018, subtracting the estimated reduction of pollutant loading as a result of sending HSW to ocean disposal, and calculating a new maximum pollutant concentration by dividing the calculated pollutant loading by the maximum observed flow.

The long-term average values were determined by first averaging available daily concentrations and loads from April to December 2018. For determining the maximum 30-day values, daily concentrations and mass loads were averaged for each full calendar month from April to December 2018. The pollutant load that is estimated to be removed from the final effluent stream after ocean disposal of HSW was then subtracted from the historical average daily pollutant load and maximum 30-day pollutant load to estimate the projected average daily load and 30-day pollutant load, respectively, once ocean disposal begins. The average load estimated in the final effluent was then divided by the average final effluent flow from the Facility after ocean disposal begins to calculate the average concentration of pollutants in the wastewater final effluent. The monthly average concentration was similarly calculated using the maximum 30-day loading and maximum 30-day wastewater final effluent flow after ocean disposal begins.

The effluent characteristics, accounting for StarKist resuming ocean disposal of the HSW, could only be estimated for constituents that are regularly sampled as part of the DMRs, plus other regularly sampled data. This includes the following: total aluminum, ammonia (as N), biological oxygen demand (5 day), total cadmium, chemical oxygen demand, total chromium, total copper, total mercury, total nickel, nitrate+nitrite (as N), TN, O&G, TP, TSS, and flow. The number of analyses reported on Form 2C for each of these aforementioned constituents (that were updated to account for ocean disposal) represents the number of historical analysis results from April through December 2018. For the remaining constituents that were not updated to reflect anticipated effluent quality after ocean disposal is resumed, the most recent available data were reported. However, this is a conservative approach, since resuming ocean diposal will remove all of the HSW that is discharged through the JCO.

Constituents with a maximum daily concentration of "ND" were analyzed for, but were not detected at or above the method reporting limit (MRL)/MDL. Maximum daily concentrations with values followed by an asterisk (\*) reflects results that were estimated values, while a value followed by two asterisks (\*\*) represents an estimated value where the reported value was from a dilution.

Analyses for radioactivity or fecal coliform were not performed. Based on input from gdc, U.S. EPA permitting staff have not required sampling for these constituents in the past. In addition, there is no laboratory in American Samoa that is able to analyze for fecal coliform and all sanitary waste from the cannery (which would be a sanitary source of fecal coliform) is conveyed to the Utulei wastewater treatment plant operated by the ASPA. In addition, the Facility has not measured total residual chlorine at the wastewater treatment effluent location. It should also be noted that the bromine system, where bromine was used in the treatment train for HSW, was decommissioned on the same day that samples were collected for the PPS analysis. Therefore, the presence of bromine in the effluent during this sampling event is likely due to the bromine system that has since been decommissioned.

Additionally, the anticipated maximum daily wastewater flow generated at the Facility is 3.0 mgd. The maximum daily flow requested for the renewed NPDES permit is 2.9 mgd, which represents the flow corresponding to the anticipated maximum daily production in the upcoming permit term with the quantity of wastewater flow subtracted representing the wastewater streams that were historically ocean disposed. This flow value is slightly higher than the maximum daily flow requested in the previous permit renewal application submitted in 2018 (2.6 mgd). The average daily wastewater flow generated at the Facility is 2.0 mgd. The average wastewater flow to the JCO in the renewed NPDES permit is 1.87 mgd, which represents the average daily wastewater flow generated at the Facility minus the anticipated quantity of wastewater to ocean disposal.

## Section V.D (Form 2C) – Potential Discharge of Substances

Under 40 CFR 117.12(a)(2), certain discharges of hazardous substances (listed in Table 2c-4 of Form 2C) may be exempted from the requirements of section 311 of the Clean Water Act (CWA), if the origin, source, and amount of the discharged substance are identified in the NPDES permit application. The information in Table 1 is included below in order to apply for an exclusion of the discharge of the substances from the requirements of section 311.

The chemicals listed Table 1 are used at different locations within the Facility, depending on the intended purpose of the chemical. Table 1 includes the estimated annual usage<sup>4</sup> of the hazardous substance. However, these values do not represent the amount of the substance that is discharged from the Facility through the JCO. Through the normal use of Facility chemicals and washdown of equipment, the substances may be collected with other wastewater generated at the Facility through process piping and drains. The Facility wastewater flows to the wastewater treatment processes for treatment prior to final discharge from the Facility and removes hazardous substances

<sup>&</sup>lt;sup>4</sup> Based on the estimated annual usage of the specified chemical and the composition of the hazardous substance in the chemical used.

as a byproduct of treating other pollutants in the wastewater. Residual chemical is neutralized with organics within the wastewater as well as from final pH adjustment before the final treated wastewater discharge. Therefore, the treatment system treating the normal Facility discharge is treating the substances before they are discharged.

**Table 1. Substance Usage at the Facility** 

Chemical Used	Hazardous Substance	Units	Estimated Annual Usage of Hazardous Substance <sup>1</sup>	Usage Area/Purpose	Potential Discharge
Sodium Hydroxide	Sodium Hydroxide <sup>2</sup>	lbs	54,263	Evaporators and air scrubbers CIP, facility sanitation	Chemical is used during CIP in the evaporators and air scrubbers once each week and during general Facility sanitation.
Sulfuric Acid	Sulfuric Acid <sup>2</sup>	lbs	32,387	Evaporators and air scrubbers CIP	Chemical is used during CIP in the evaporators and air scrubbers once each week and during general Facility sanitation.
Sodium Hypochlorite	Sodium Hypochlorite <sup>2</sup>	lbs	18,100	General sanitation, thaw water, retort system, evaporators and air scrubbers CIP	Chemical is used during CIP in the evaporators and air scrubbers once each week and during general Facility sanitation. In addition, chemical is used to disinfect the thaw water and retort water.
Sodium Hypochlorite	Sodium Hydroxide <sup>2</sup>	lbs	1,378	General sanitation, thaw water, retort system, evaporators and air scrubbers CIP	Chemical is used during CIP in the evaporators and air scrubbers once each week and during general Facility sanitation. In addition, chemical is used to disinfect the thaw water and retort water.
Quorum Copper	Sodium Hydroxide <sup>2</sup>	lbs	9,936	Facility sanitation	Chemical is used for Facility sanitation.
Quorum Green	Sodium Hypochlorite <sup>2</sup>	lbs	2,526	Facility sanitation	Chemical is used for Facility sanitation.
Quorum Green	Sodium Hydroxide <sup>2</sup>	lbs	289	Facility sanitation	Chemical is used for Facility sanitation.
AC-103	Sodium Hydroxide <sup>2</sup>	lbs	36,334	Facility sanitation	Chemical is used for Facility sanitation.
PCC Alkali	Sodium Hydroxide <sup>2</sup>	lbs	16,579	Facility sanitation	Chemical is used for Facility sanitation.
HD LC-30	Phosphoric Acid <sup>2</sup>	gallon	74	Facility sanitation	Chemical is used for Facility sanitation.
Filtrapure Liquid Acid Cleaner	Phosphoric Acid <sup>2</sup>	lbs	244	Retort water RO system	Used intermittently as a cleaner in the Retort RO system to restore membrane permeability. Trace amounts of chemical may be discharged to the wastewater treatment collection system.

Chemical Used	Hazardous Substance	Units	Estimated Annual Usage of Hazardous Substance <sup>1</sup>	Usage Area/Purpose	Potential Discharge
Filtrapure Liquid TF Cleaner	Sodium Hydroxide <sup>2</sup>	lbs	64	Retort water RO system	Used intermittently as a cleaner in the Retort RO system to restore membrane permeability. Trace amounts of chemical may be discharged to the wastewater treatment collection system.
Filtrapure FG BS	Sodium Bisulfite	lbs	3,598	Retort water RO system	Used to depress the oxidation/reduction potential in the RO influent. Trace amounts of chemical may be discharged to the wastewater treatment collection system.
Aluminum sulfate	Aluminum Sulfate	lbs	374,886	Wastewater DAF system	Aluminum sulfate is used to settle out organic solids in the DAF wastewater treatment process. Aluminum is predominantly removed from the wastewater as sludge.
Sunbugger 100	Pyrethrins	lbs	3.7	Facility pest control	Chemical is diluted and fogged throughout the Facility and warehouse to deter rodents and pests. Small quantities of residual chemical may be washed from equipment surfaces and collected in the wastewater collection system. However, chemical is being treated by the DAF <sup>2</sup> .
Demand CS	Xylene	lbs	0.011	Facility pest control	Chemical is diluted and fogged throughout the Facility and warehouse to deter rodents and pests. Small quantities of residual chemical may be washed from equipment surfaces and collected in the wastewater collection system.
Acid Wash FG	Phosphoric Acid <sup>2</sup>	lbs	11,885	Facility sanitation	Chemical is used for Facility sanitation.
Termin8	Propionic Acid	lbs	8,220	Fishmeal process	Chemical is self-contained in the fishmeal process. Trace amounts of residual chemical from overspray of chemical may be collected in the wastewater collection system.
Termin8	Formaldehyde	lbs	30,140	Fishmeal process	Chemical is self contained in the fishmeal process. Trace amounts of residual chemical from overspray of chemical may be collected in the wastewater collection system.

Chemical Used	Hazardous Substance	Units	Estimated Annual Usage of Hazardous Substance <sup>1</sup>	Usage Area/Purpose	Potential Discharge
Nalco 19 PULV	Sodium Bisulfite (equivalents, from Sodium Metabisulfite)	lbs	45.3	Boiler	Used as a oxygen scavenger for corrosion control in the boilers. Trace amounts of chemical may be discharged to the wastewater treatment collection system.
FoodPro ST8069	Sodium Hydroxide <sup>2</sup>	lbs	18	Can washer	Used as a corrosion inhibitor on cans prior to packaging for shipment.
FoodPro ST8069	Potassium Hydroxide <sup>2</sup>	lbs	78	Can Washer	Used as a corrosion inhibitor on cans prior to packaging for shipment
CrystalFloc B660H Polymer	Adipic Acid	lbs	1,651	Wastewater DAF system	Chemical is used to settle out organic solids in the DAF wastewater treatment process. Polymer is predominantly removed from the wastewater as sludge.

<sup>&</sup>lt;sup>1</sup>These values do not represent the amount of the substance that is discharged from the Facility through the JCO or would be discharged with ocean disposal. The Facility wastewater effluent flows to the wastewater treatment processes for treatment prior to final discharge from the Facility and removes hazardous substances as a byproduct of treating other water pollutants in the wastewater.

<sup>&</sup>lt;sup>2</sup> Residual chemical is collected with wastewater generated at the Facility through process piping and drains, and either consumed or neutralized by organics within the wastewater, or from final pH adjustment before the final wastewater outfall.

<sup>&</sup>lt;sup>3</sup> There is evidence to show that wastewater treatment can remove majority of pyrethrins by wastewater processes that remove oil and grease and suspended solids from wastewater. Pyrethrins are anticipated to accumulate in the sludge.

## POLLUTION MINIMIZATION PLANS

#### **Metals PMP Evaluation**

Geosyntec conducted a review of the metals Pollution Minimization Plan (PMP) submitted by gdc to the U.S. EPA on December 14, 2010, along with the supplement dated July 28, 2011, to assess conformance with PMP requirements as prescribed in the NPDES permit. The goal of the PMP, as stated in the NPDES permit, was to achieve water quality standards in the discharge for copper, zinc, and mercury as soon as practicable with a minimally sized mixing zone. Based on JCO effluent monitoring results for copper, zinc, and mercury collected between May 2008 and September 2010, gdc's PMP states that mercury and zinc are typically above water quality standards, while copper is typically below water quality standards; however copper does have the potential to exceed the standards. The PMP concludes that the water quality standards for copper, zinc, and mercury are met within a few seconds after discharge from the diffuser in a mixing zone that extends only a few meters from the diffuser. Therefore, the goal does appear to have been met, since gdc's PMP states that the mixing zone is very small (only a few meters from the diffuser) and that water quality standards are met within a few seconds after discharge. More detail on Geosyntec's review is summarized in the following paragraphs.

The PMP prepared by gdc was based on sampling conducted within the Facility in September 2010 and March 2011 at nine sample locations associated with low strength wastewater (LSW):

- Fresh Water Supply;
- Seawater Supply;
- Thaw Water Outflow;
- Butchering Outflow;
- Spray Cooling Outflow;
- Can Washer Outflow;
- Boiler Blowdown;
- Washdown; and
- Outfall Effluent.

At the time the PMP for metals was developed the high strength wastewater (HSW) was collected in the HSW tank and discharged to the ocean several miles off-shore via a dedicated vessel. Therefore, samples associated with HSW streams were not included in the gdc PMP.

Since the PMP was prepared, the Facility in coordination with the U.S. EPA ceased ocean discharge of the HSW in 2012 and redirected it to an on-site treatment system. A review of the data post ocean discharge of HSW identified a significant increase in the copper, zinc, and mercury concentrations<sup>5</sup> in the Facility's final effluent, as shown in Table 2. Despite these increases, the final effluent concentrations of copper, zinc, and mercury continued to be below the effective NPDES permit limits identified in Table 2. Upgrades to the wastewater treatment system were recently implemented recently. Concentrations of copper, zinc, and mercury in the Facility's

<sup>&</sup>lt;sup>5</sup> As sampled during semi-annual JCO toxicity testing.

effluent significantly decreased (from the post-HSW time period) after treatment upgrades were implemented, as shown in Table 2. The samples were collected as flow-weighted composites over a 24-hour period.

Table 2: Average Metals Values in Facility Effluent, 2008 to Present

E	Datas	Coppe	er μg/L	Zinc	μg/L	Mercu	ry μg/L
Era	Dates	Average	Max	Average	Max	Average	Max
Pre-PMP	May 2008 to December 2010	2.23	3.1	162	263	0.11	0.16
Pre-HSW (Post-PMP)	January 2011 to June 2012	2.24	2.4	102	118	$0.09^{1}$	0.16
Post-HSW	July 2012 to February 2016	11.95	18.1	459	818	0.25	0.70
Post-HSW and Treatment upgrades	March to December 2018	1.5	2.3	53.4	111	0.15	0.21
ASWQS		3.	73	85.	.62	0.0	050
NPDES Daily M	laximum Limit		117.22		2,284		4.72
NPDES Monthly	Average Limit		58.42		1,138		1.8

<sup>&</sup>lt;sup>1</sup> Daily average contains a mercury result that was non-detect; therefore, the calculation assumes half of the reporting limit for the non-detect result.

The original gdc metals PMP and supplement, which evaluated concentrations of mercury, copper, and zinc, presented the following conclusions:

- The source of mercury was attributed to the tuna;
- The primary source of copper was attributed to the tuna; and
- The primary source of zinc was attributed to the tuna and also galvanized fish boxes and other equipment. The report further states that galvanized equipment is necessary in a marine environment to avoid excessive corrosion.

The gdc PMP states that since the tuna was identified as the primary source of each metal evaluated, and further stated that there is no practicable way to reduce these in-plant sources other than maintaining good housekeeping practices. These practices should involve the clean-up of scrap that is removed during washdown activities, a recommendation that originated in gdc's PMP. The gdc PMP also noted that the unavoidable and uncontrollable concentrations of mercury, copper, and zinc in the final effluent from the Facility can be addressed by appropriate NPDES permit limitations and maintaining an approved mixing zone. The gdc PMP states that the mixing zones for these parameters are very small, extending only a few meters from the diffuser and at depths below 150 feet. Therefore, since effluent limits continue to be met based on an approved mixing zone, water quality standards presumably continue to be achieved in the receiving water within a few seconds after (and meters of) discharge. Semi-annual JCO receiving water quality monitoring reports confirm this ongoing condition of acceptable receiving water quality for these constituents.

Table 2 also demonstrates that the metals PMP recommended actions may have resulted in a decrease in effluent zinc concentrations, though no post-PMP decreases were observed for copper

or mercury, and the post-PMP zinc improvements were negated after inclusion of HSW. These temporary zinc reductions may be attributed to change-out or replacement of some of the galvanized equipment used by the Facility, natural variation in the metals content of incoming fish tissue, or some combination thereof.

Implementation of recent measures has also had an impact on the metals concentrations in the final discharge since a significant portion of the fish solids was removed from the HSW stream. The impact of upgrades is exhibited in the sampling results from 2018 (Table 2), which showed a significant decrease in copper, zinc, and mercury concentrations from the post-HSW scenario to the post-HSW and treatment upgrades scenario.

With respect to non-metal constituents, introduction of the HSW treatment system effluent to the Facility's final effluent discharge point also impacted the final effluent concentration of nutrients (total phosphorus, total nitrogen, and ammonia), total suspended solids, and oil and grease significantly. The following subsection discusses a PMP associated with the reduction of these constituents.

### **Nutrients PMP**

Since the introduction of HSW treatment system effluent to the Facility's final effluent stream in June 2012, StarKist has been challenged to reduce the concentrations of the following constituents in their final effluent:

- Ammonia;
- TN;
- TP;
- O&G; and
- TSS.

In support of reducing final effluent contamination from the Facility, Geosyntec completed on-site sampling and flow monitoring in July and September 2015 to collect data on the existing systems and processes within the Facility. Geosyntec completed an Environmental Summary Report, which was issued to StarKist, Eckert Seamans, and the U.S. EPA on December 21, 2015, describing the observations made during two Facility visits completed in July and September 2015, and the results of sampling conducted during the September 2015 visit. Many treatment system upgrades were implemented to improve effluent TN and TP loadings. A wastewater sampling event to quantify the improvements to the wastewater effluent associated with the upgrades was conducted, and a report summarizing the impacts of the upgrades on the final effluent wastewater characteristics was submitted on May 01, 2018. From that point, further evaluation will assess whether additional upgrades to the treatment system will be required.